Scenario earthquake- Link of Probabilistic and Deterministic SHA's

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Why combine the two

- Engineering seismic hazard assessment, so called PSHA, is now widely adopted in zoning maps at national, regional and city level in the world.
- In probabilistic seismic hazard assessment, ground motion from earthquake with magnitude in interval M_j and in kth potential area is estimated by means of attenuation relationship.
- The attenuation relation is a kind of simplification, taking magnitude for source mechanism, distance for path of wave propagation, and the source is considered as a point.
- Ground motion at the near field of large earthquake must be overestimated or underestimated, since the energy from a quite large source (rupture plane) is concentrated on a point (hypocenter).

Why combine the two (cont. 1)

- Strong ground motion at near field is well known complicated since it is governed by the source predominately and the source of large earthquake is quite complicated in general.
- In that case, a rupture plane is needed to characterize the source, for otherwise the ground motion tends to be overestimated, and the near fault effect cannot be simulated.
- Finite fault model is currently adopted in strong ground motion simulation to describe near-fault rupture directivity effect and hanging wall effect which strongly influence the distribution of ground motion amplitudes on rock sites in the near fault region.

Why combine the two (cont. 2)

- A new idea is proposed to combine the two approaches, the key step is how to establish a link between the two.
- Benefit of seismic zoning map is mainly from mitigation of loss and casualty in cities in large earthquake.
- To describe the probabilistic seismic hazard of a city, scenario earthquake is widely adopted, with some strong queries, since the difference between hazard from an earthquake and that from earthquakes with various magnitudes in many areas.

How to build a link

- The way to deal with a scenario earthquake is the key step to build a link between PSHA and DSHA.
- This is seismic hazard curves of a city in case study by PSHA



Uncertainty correction of seismic hazard



潜源编号	10.00	40.00	80.00	120.00	160.00	200.00	250.00	300.00	400.00	600.00	
1	0. 0010	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2	0.0005	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
3	0.0002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
4	0.0058	0.0001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
5	0.0011	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
6	0.0165	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1
7	0.0065	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
9	0. 0015	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
10	0. 0017	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
12	0.0081	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
13	0.0083	0. 0018	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
14	0.0003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
15	0. 0120	0.0024	0.0005	0.0001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
16	0. 0121	0.0009	0.0001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
17	0.0060	0.0005	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
19	0.0024	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
20 ┥	0.0627	0. 0159	0.0068	0.0034	0.0017	0.0008	0.0002	0.0000	0.0000	0.0000	
21	0. 0200	0.0027	0.0003	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
22	0. 0033	0.0001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
24	0. 0021	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
25	0. 0210	0.0040	0.0008	0.0002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
26	0.0028	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
27	0.0007	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
28	0.0025	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
29	0.0040	0.0002	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
30	0. 0038	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
31	0.0006	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
32	0.0010	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
33	0.0005	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
34	0.0066	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
36	0.0008	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
37	0.0001	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	

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							-







Exceeding Probability	63% in 50 years	10% in 50 years	2% in 50 years
PGA (gal)	59	192	345
Magnitude	5.7	6.5	7.0
Distance (km)	30	21	16
Causative fault	Maxianshan North Fault	Western segment of Maxianshan North Fault	Midele and Eastern segments of Maxianshan North Fault

Parameter	Magnitude 6.5	Mean value
Rupture area 🙎	$\log S = M_w - 4.0$	136 km²
Rupture width W	$\log W = 0.5 M_{\psi} - 2.125$	8 km
Rupture length L	$L = \frac{S}{W}$	17 km
Average slip on the rupture \overline{D}	$\log \overline{D} = 0.5 M_{\psi} - 1.45$	146 cm





Parameter	Max. Asperity	Other Asperity
Asperity area (km²)	$\log S_{am} = \log S - 0.92$	$\log S_a = \log S - 0.65$ $S_{ao} = S_a - S_{am}$
Asperity length (km)	$\log L_{a_m} = 0.5L - 2.31$	$L_{ao} = \frac{S_{ao}}{W_{ao}}$
Asperity width (km)	$W_{am} = \frac{S_{am}}{L_{am}}$	$W_{ao}=\!\xi_{_W}\sqrt{S_{_{ao}}}$
X coordinate of Asperity center (km)	$\log x_{am} = \log L - 0.72$	$X_{ao} = \xi_{\mathcal{X}} (L - X_2)$
Y coordinate of Asperity center (km)	$\log y_{am} = \log W - 0.28$	$Y_{ao} = \xi_W imes W + W_{ao} / 2$
Average slip of Asperity (cm)	$\log \overline{D}_{am} = \log \overline{D} + 0.39$	$\log \overline{D}_{ao} = M_w + 0.31$



Magnitude 6.5	Mean value
$\log k_{cx} = 1.89 - 0.5 M_w$	0.0437
$\log k_{cy} = 2.09 - 0.5M_w$	0.0692

$$D(k_x, k_y) = \frac{\overline{D} \cdot L \cdot W}{\sqrt{1 + \left(\left(\frac{k_x}{k_{cx}}\right)^2 + \left(\frac{k_y}{k_{cy}}\right)^2\right)^2}} e^{i\Phi(k_x, k_y)}$$















Conclusion

- A new idea is proposed to combine the PSHA and DSHA approaches for the next generation map.
- Scenario earthquake is emphasized as the key step to establish a link between the two.
- From a case study, the detail hazard result by mean attenuation relation is examined, and the most potential source area is acquired for a given exceeding probability.
- A distance range is then fixed from the segmentation of the main active fault in the source area, and the corresponding magnitude is calculated from the PGA by PSHA by the mean attenuation law.
- The magnitude is checked from the upper bond magnitude of the potential area.

Conclusion (cont.1)

- Finite fault source model is built from the checked magnitude with the fault data as much as possible.
- 30 source models are presented to take into account uncertainty on global and local parameters.
- The ground motions at near field are synthesized, and average PGA is assigned to each rock site, and soil site as well by taking site condition into account further.
- The isoseismials constructed from the synthesized motion field is overlaid on that from PSHA, and the two are merged together as the final map by replacing the PSHA result at near field by the synthesized one.

Conclusion (cont.2)

- By this way, the scenario is the maximum confidential, from seismotectonic condition, the corresponding PGA by mean attenuation relation is the same as the PSHA result by the same relation.
- In this meaning, the isoseismals from the scenarion could be considered with that exceeding probability of the PSHA result, and can merged with that together.
- The uncertinty on source model has been taken into account, and that on attenuation could also be taken into account by the same way to synthesize more motion fields from each source model with different values of random error term in attenuation law.
- The hign intensity area on the map is shifted now westwards reasonably as an improvement.
- The number of synthesis is determined by the stability of the mean PGA.



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Seismic hazard of a city by PSHA



