" $V_{S\,30}$ - A Basis for Characterization of Seismic Site Response for Site-specific, Regional, and Global Mapping of Seismic Hazard

Roger D. Borcherdt

1st Annual Meeting of the Strategic Chinese-Korean-Japanese Cooperative Program: Seismic Hazard Assessment for the Next Generation Map

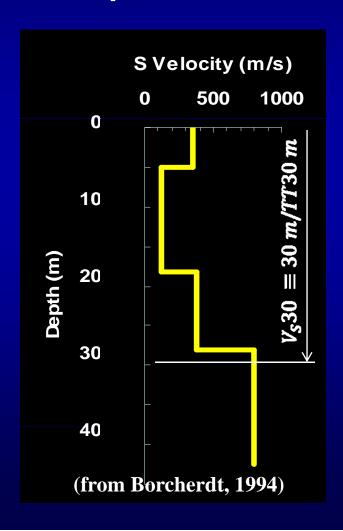
> November 25-30, 2011 Harbin Institute of Technology Harbin, China

Outline

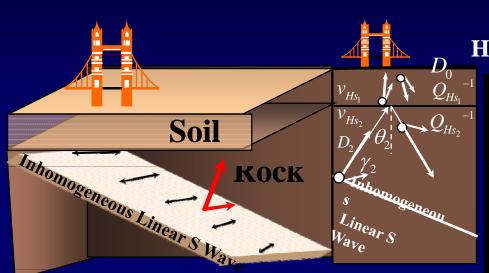
- Definition V_{S30}
- $V_{S\,30}$ as a Basis for Characterization of Site-Specific Site Response
 - Theoretical Dependence of Amplification on V_{S30}
 - Empirical Dependence of Amplification on V_{S30}
 - V_{adj} correlations with V_{adj} at other depths
- V_{S30} as a Basis for Mapping Site Response Correlations of V_{S30} with:
 - Physical Properties -- Site Class definitions
 - Geologic Age
 - Topographic Slope
- Applications of $V_{S\,30}$
 - Site-Specific Response Characterization Site Classes, Site Coefficients, Building Codes
 - Regional Site Response Mapping GMPEs, ShakeMaps, PSHA, GEM

$\overline{V_{S30}}$ Definition

 $V_S30 \equiv 30 \, m/Travel \, time \, to \, 30 \, m$



Theoretical Response of a Viscoelastic Soil Layer versus Vs Ratio and Normalized Freguenc



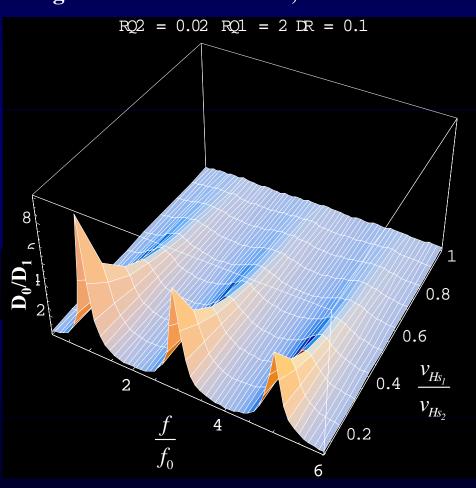
Amplitude Response versus Frequency Homogeneous Linear S Wave, Vertical Incidenc

Solution:

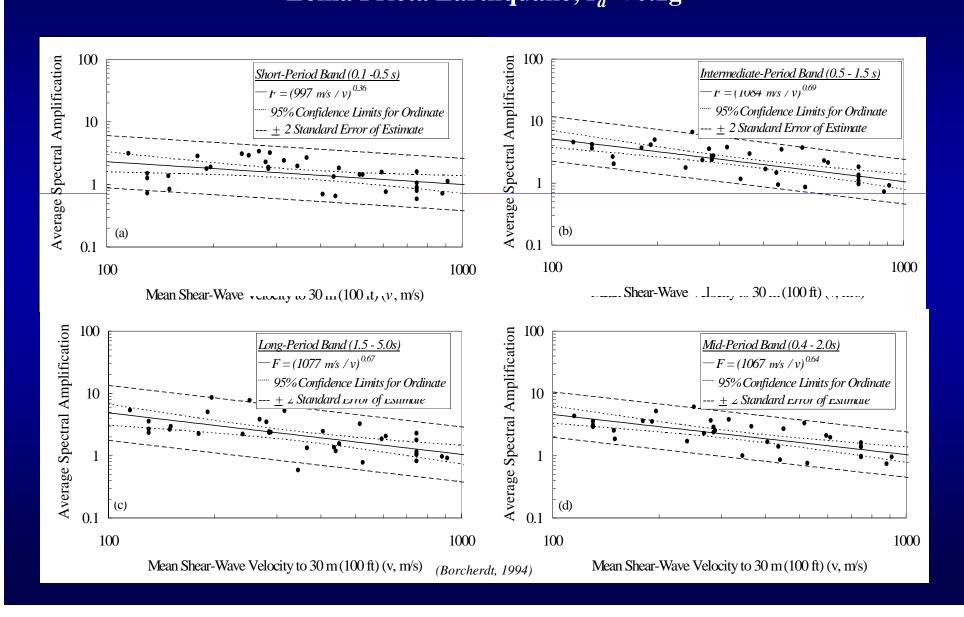
$$\frac{D_0}{D_1}$$
 = F[(inc. wave field par.),(material par.)]

$$\frac{D_0}{D_1} = F[(\theta_2, Q_{Hs_1}, Q_{Hs_2}, Q_{Hs_1}, Q_{Hs_2}, Q_$$

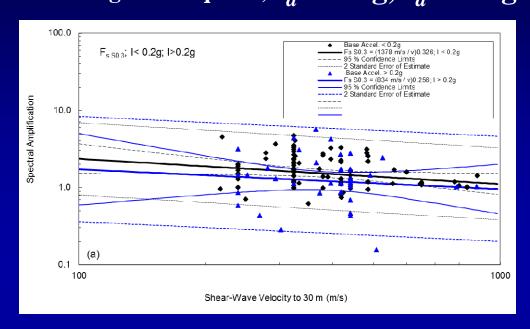
where f_0 =fundamental frequency.

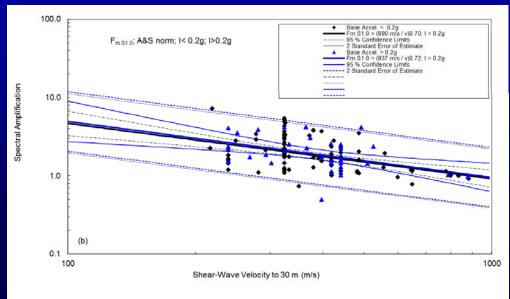


Empirical Spectral Amplification Values versus $V_{S\,30}$ Loma prieta Bartinquake; I_a < 0.19



Empirical Spectral Amplification Values versus $V_{S\,30}$ Northridge Earthquake; $I_a < 0.2 {\rm g}, I_a > 0.2 {\rm g}$





Empirical Dependence of Amplification on $V_{S\,30}$

(Site Coefficients for Seismic Design)

Short- and Mid-Period Amplification Factors are:

$$F_a = (V_{ref}/V_{S30})$$

and

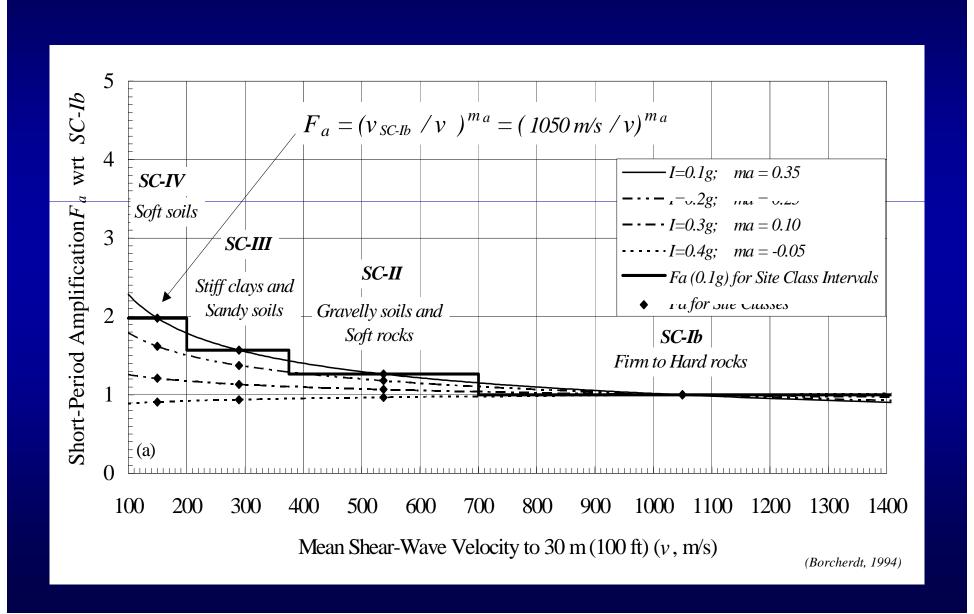
$$F_v = (V_{ref}/V_{S30})$$

where,

- 1) V_{S30} is inferred or measured mean shear-wave velocity to 30 m at site,
- 2) V_{ref} is V_{S30} for reference ground condition,
- 3) m_a and m_v depend on input ground motion level.

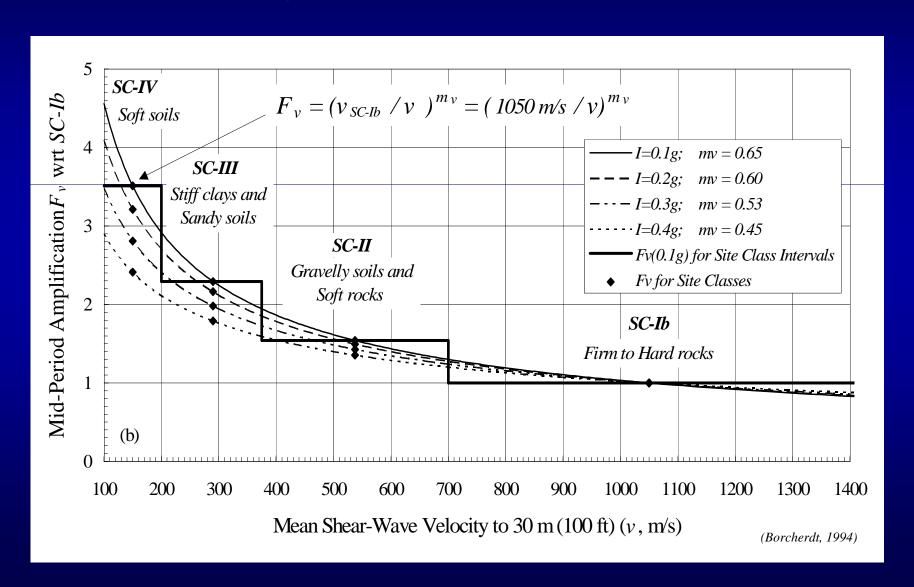
F_a versus Input Amplitude & V_{S30}

 $I_a = 0.1, 0.2, 0.3, 0.4 \text{ g}$ (linear scales)

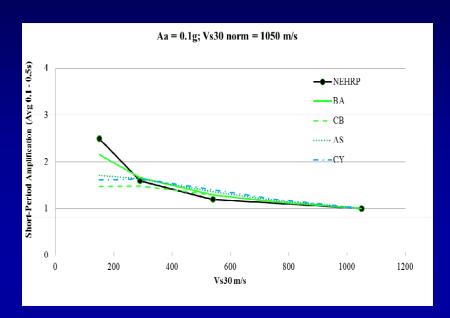


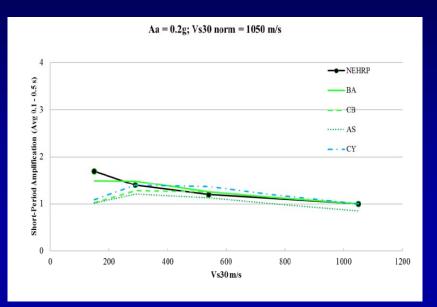
F_{v} versus Input Amplitude & V_{S30}

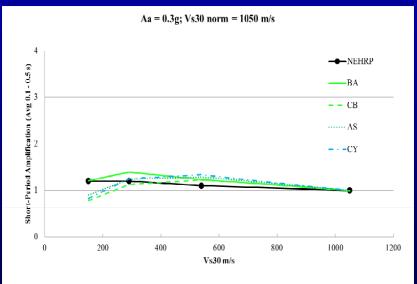
 $I_v = 0.1, 0.2, 0.3, 0.4 \text{ g (linear scales)}$

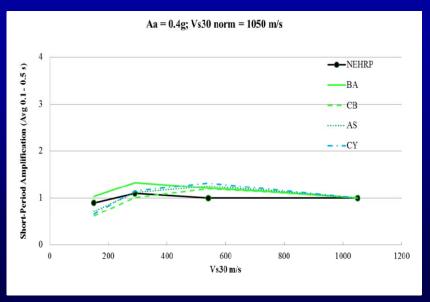


NEHRP & NGA Short-Period Amplification versus $V_{S\,30}$ Aa=0.1g; Avg. 0.1-0.5s; Vs30 norm 1050 m/s

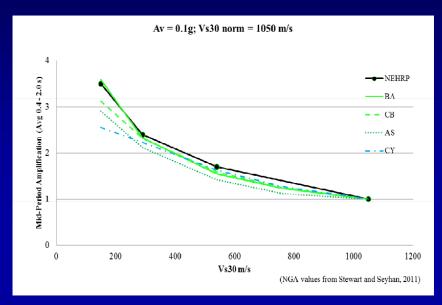


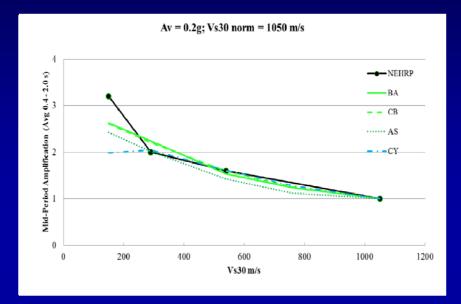


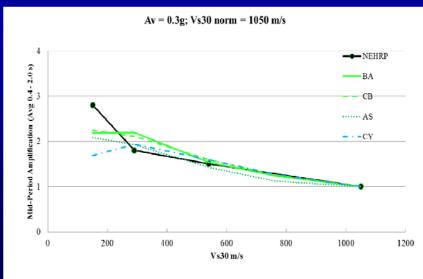


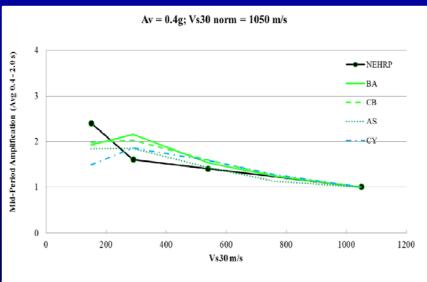


NEHRP & NGA Mid-Period Amplification versus $V_{S\,30}$ Av = 0.1g; Avg. 0.4-2.0 s; Vs30 norm 1050 m/s









V_{S30} Correlation with V_{SZ} at other Depths

 V_{S30} as a function of V_{SZ} at another depth:

$$Log[V_{S30}] = c_0 + c_1 \ Log[V_{SZ}] = G(V_{SZ})$$
(Cadet, et al., 2009; Boore, et al., 2011)

Hence, amplification as a function of $V_{S\,3\theta}$:

$$m_a$$
 $F_a = (V_{S30 \, ref} / V_{S30}) = F_a (V_{S30 \, ref}, V_{S30})$

Implies amplification as a function of $V_{S\,Z}$ at other depths:

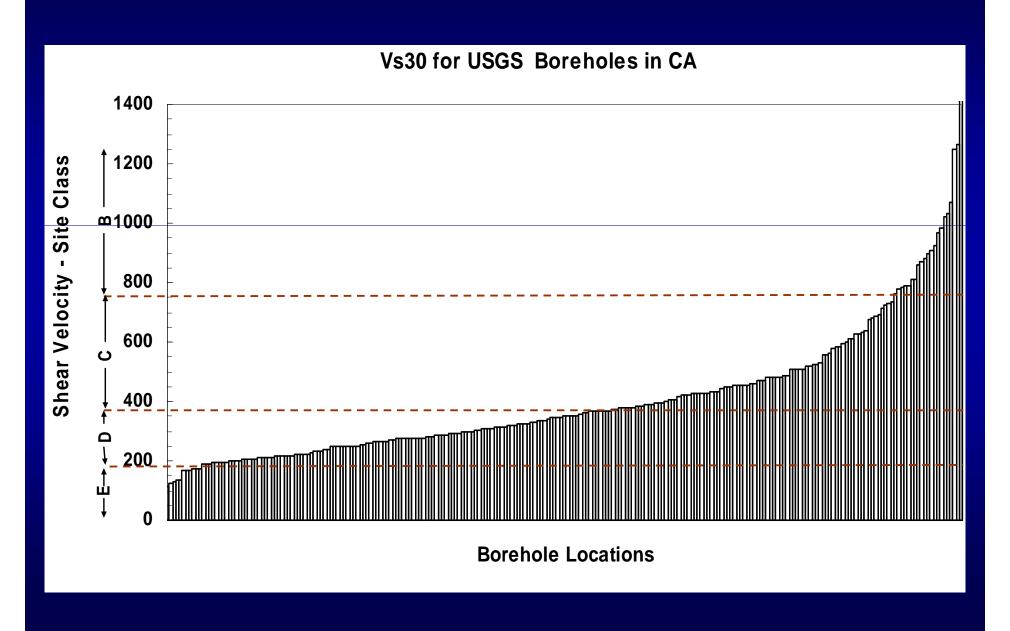
$$F_a = H_a(V_{SZref}, V_{SZ})$$

$\overline{V_{S30}}$ as a Basis for Mapping Site Response

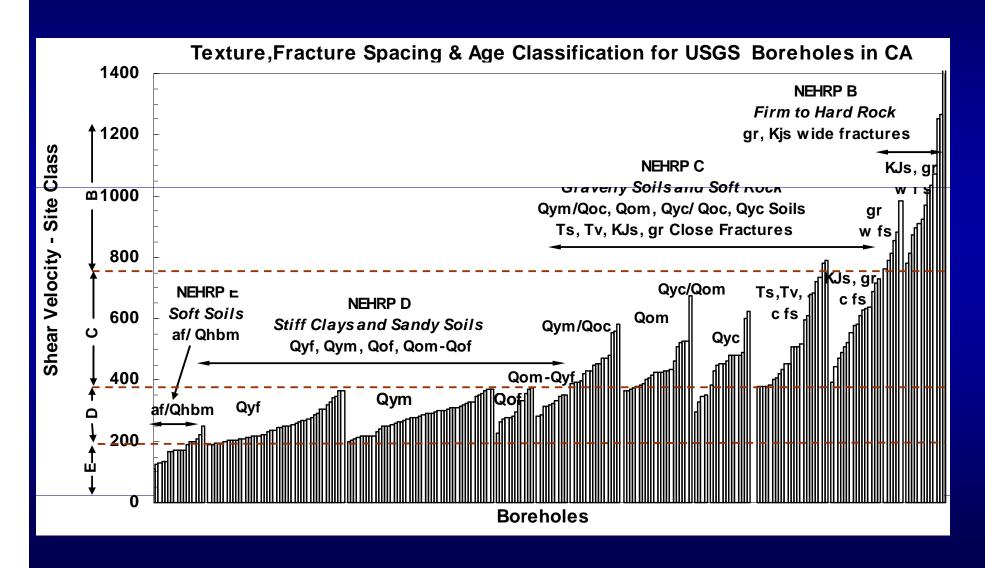
Correlations of $V_{3,3}$ with:

- ➤ Physical Properties -- Site Class definitions
- > Geologic Age
- > Topographic Slope

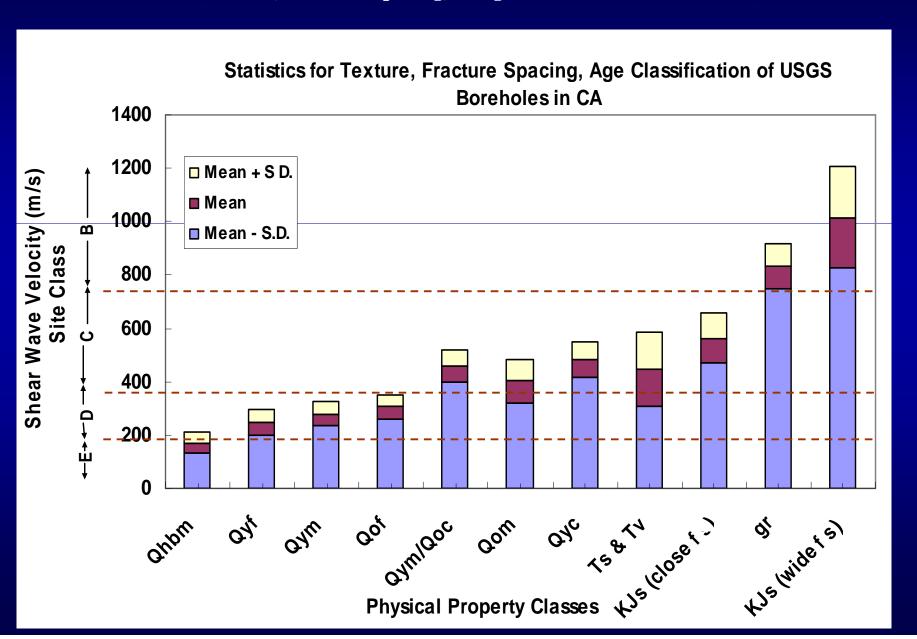
V_{S 30} for USGS Boreholes in CA



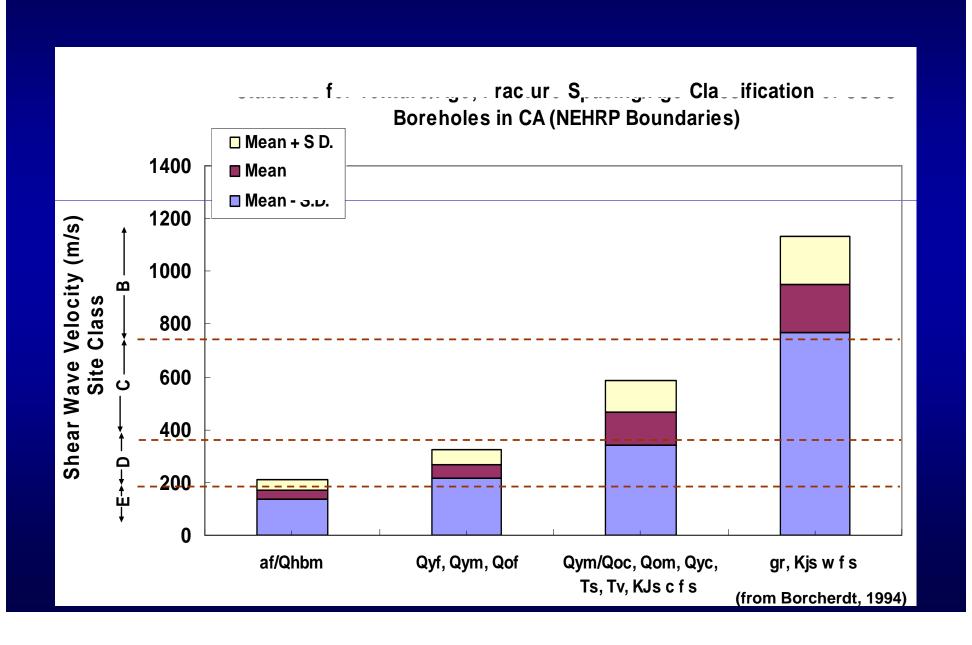
$\overline{V_{S\,30}}$ versus Physical Property Classification for USGS Boreholes in CA Suggests Seismically Distinct Units



$V_{S\,30}$ Statistics for Physical Property Classification (Texture, Fracture Spacing, & Age -- USGS Boreholes in CA)

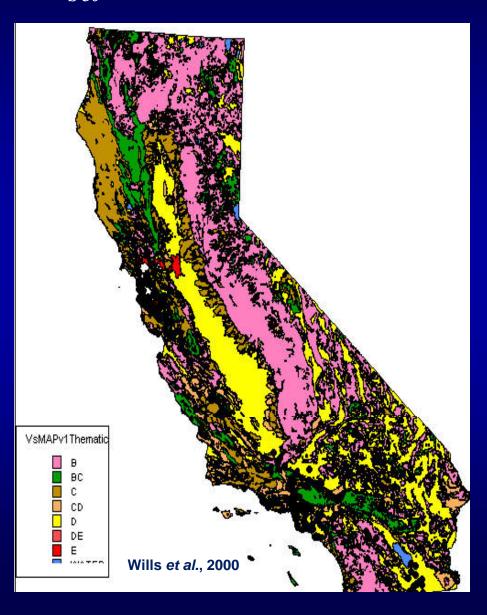


Vs30 Statistics for Physical Property NEHRP Site Classes (Texture, Fracture Spacing, & Age -- USGS Boreholes in CA)

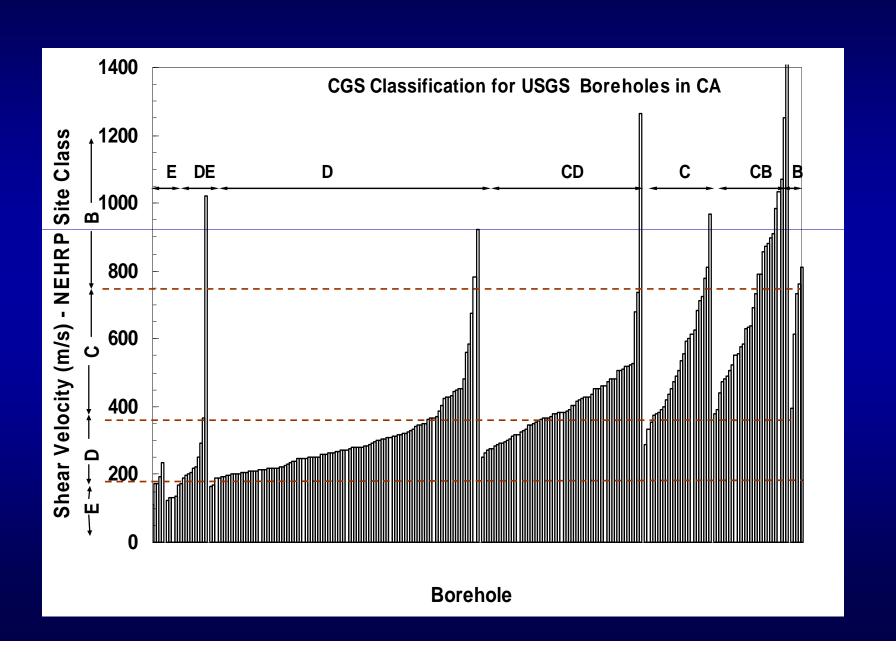


Geologic Site Condition Map

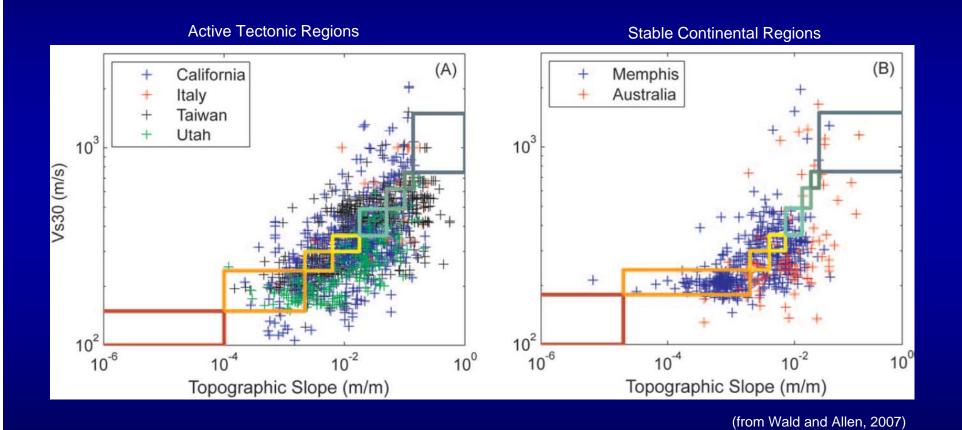
 $(V_{S30}$ correlations with Geologic Age)



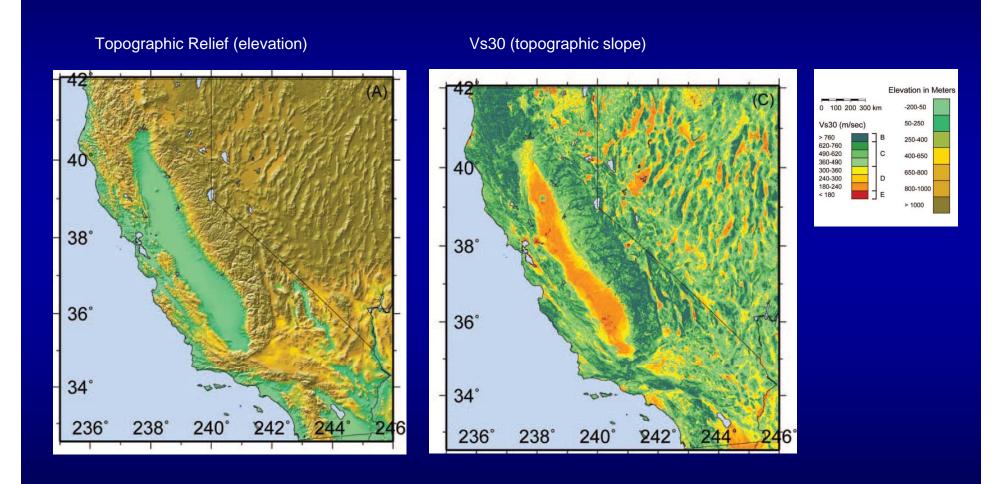
CGS Geologic Classification versus $\overline{V_{S\,30}}$



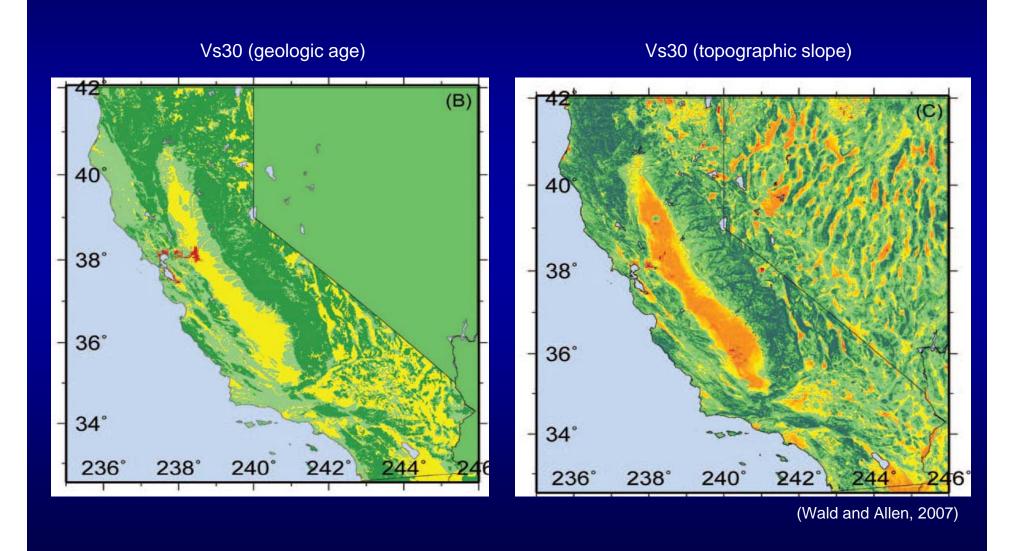
V_{S30} Correlations with Topographic Slope



$V_{S\,30}\,{ m Map}$ (Derived from Topographic Slope)



$V_{S\,30}$ Maps (Derived from Geologic Age and Topographic Slope)

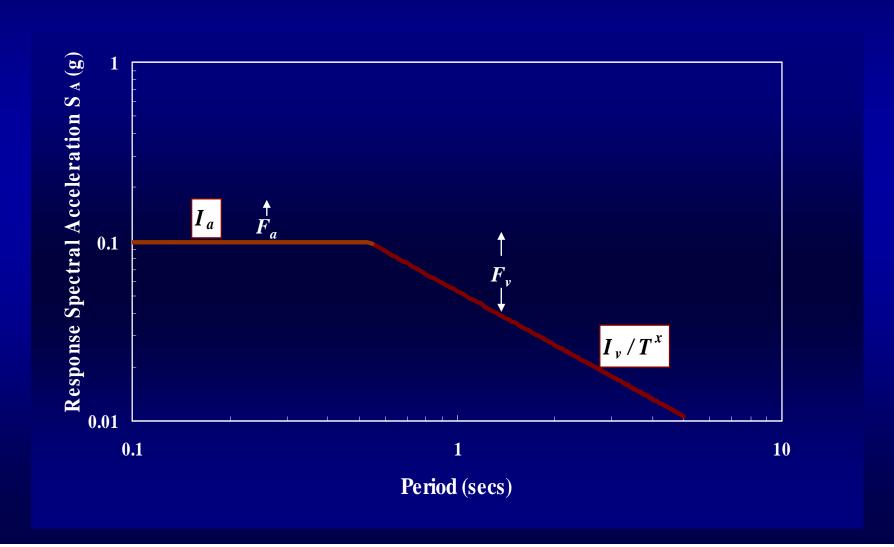


Applications of V_{S30}

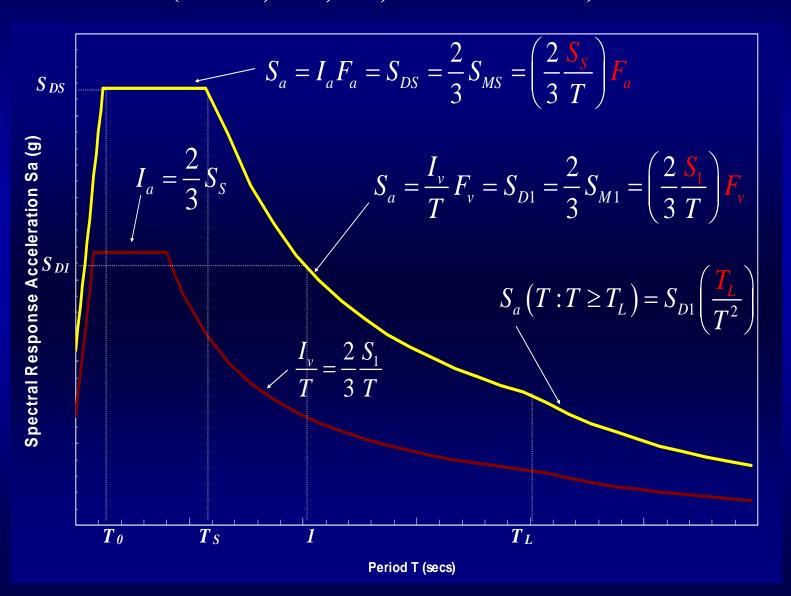
- Site-Specific Response Characterization
 - Site Classes & Site Coefficients for Site-specific Design Spectra, Building Codes
 - Ground Motion Prediction Equations (GMPE) developed as continuous function of Vs30
- Re ional Site Res onse Map in
 - ShakeMaps
 - PSHA Maps
 - Global Earth _uake Model GEM

Definition of Site-Dependent Response Spectra (log-log scale)

(NEHRP, UBC, IBC, ASCE 7 Provisions)

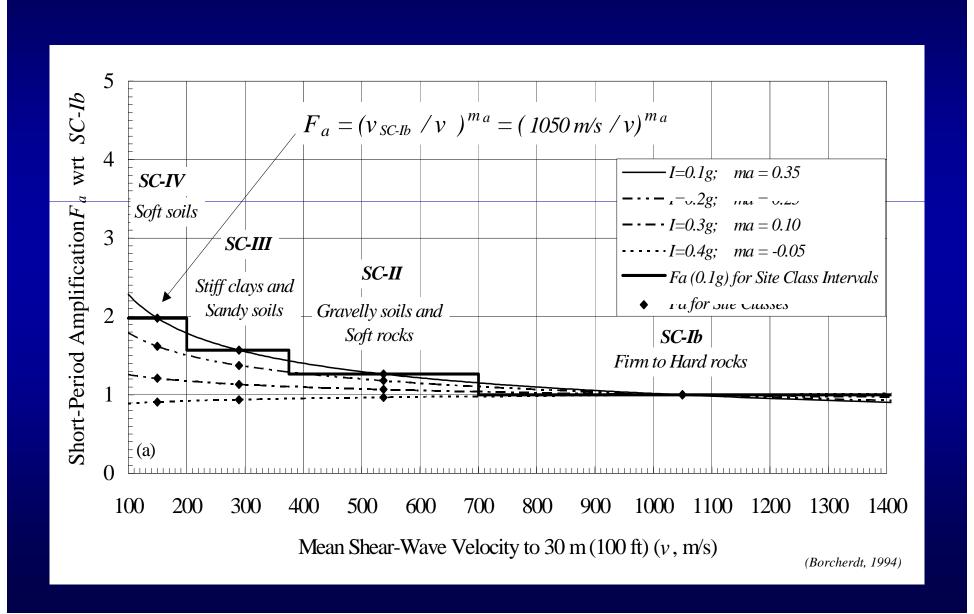


Site-Dependent Response Spectra (linear-linear scale) (NEHRP, UBC, IBC, ASCE 7 Provisions)



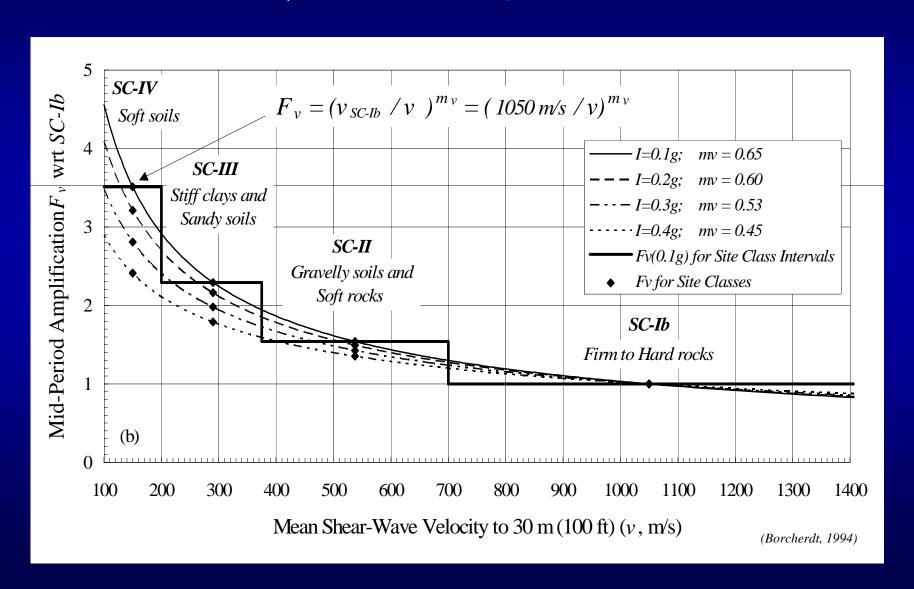
F_a versus Input Amplitude & V_{S30}

 $I_a = 0.1, 0.2, 0.3, 0.4 \text{ g}$ (linear scales)



F_{v} versus Input Amplitude & V_{S30}

 $I_v = 0.1, 0.2, 0.3, 0.4 \text{ g (linear scales)}$



Short-Period Site Coefficient F_a (NEHRP, UBC, IBC, AASHTO, ASCE 7 Provisions)

Site	$A_a \leq 0.1$	$A_a = 0.20$	$A_a = 0.30$	$A_a = 0.40$	$A_a \ge 0.50$
Class	$S_s < 0.25$	$S_s = 0.50$	$S_s = 0.75$	$S_s = 1.00$	$S_s \ge 1.25$
A	0.8	0.8	0.8	0.8	0.8
В	1.0	1.0	1.0	1.0	1.0
C	1.2	1.2	1.1	1.0	1.0
D	1.6	1.4	1.2	1.1	1.0
E	2.5	1.7	1.2	0.9	*
F	*	*	*	*	*

^{*} Site-specific geotechnical investigation and dynamic site response analysis shall be performed.

Mid-Perio_ Site Coefficient F_{ν}

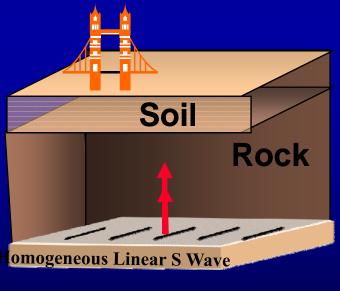
(NEHRP, UBC, IBC, AASHTO Provisions)

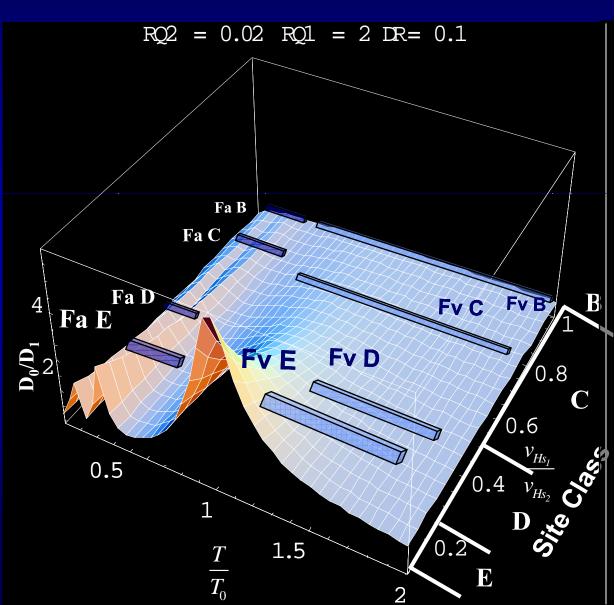
Site	$A_{v} \leq 0.1$	$A_{\nu}=0.20$	$A_{\nu}=0.30$	$A_{\nu}=0.40$	$A_{\nu} \geq 0.50$
Class	$S_l < 0.1$	$S_l = 0.20$	$S_l = 0.30$	$S_l = 0.40$	$S_l \ge 0.50$
A	0.8	0.8	0.8	0.8	0.8
В	1.0	1.0	1.0	1.0	1.0
C	1.7	1.6	1.5	1.4	1.3
D	2.4	2.0	1.8	1.6	1.5
E	3.5	3.2	2.8	2.4	*
F	*	*	*	*	*

^{*} Site-specific geotechnical investigation and dynamic site response analysis shall be performed.

Response versus Period, Shear Velocity, and Code Site Class

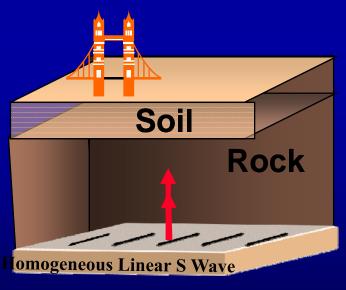
Anelastic Soil Layer Damping Ratio 5% Vertical Incidence

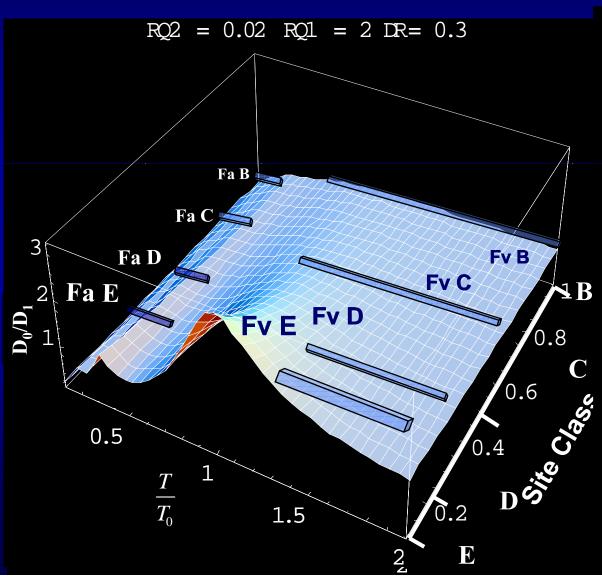




Code Site Coefficients and Theoretical Response 15 % Damping or I_a~ v.4 g

Anelastic Soil Layer
Damping Ratio 15 %
la ~0.4 g
Vertical Incidence





NGA Ground Motion Prediction Equations

$$\mathbf{GMPE} = f(V_{S30})$$

GMPE

$$\ln Y = f_{mag} + f_{dis} + f_{style of faulting} + f_{site} + f_{sed} + \varepsilon$$

Where, site condition term = $f_{site}(V_{s30})$

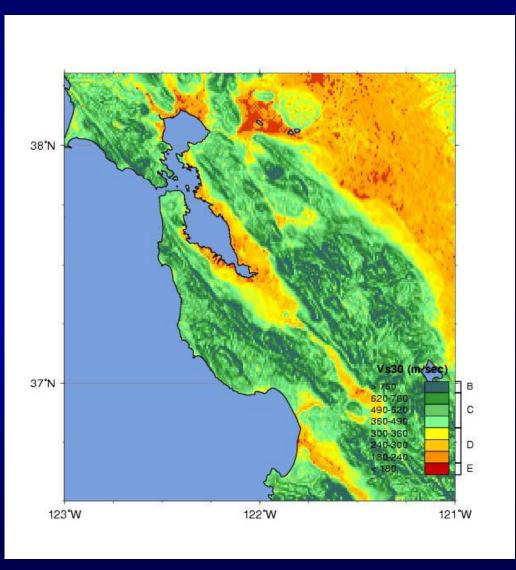
$$f_{site} = \begin{cases} c_{10} \ln \left(\frac{\mathbf{V}_{s30}}{k_1} \right) + k_2 \left\{ \ln \left[A_{1100} + c \left(\frac{\mathbf{V}_{s30}}{k_1} \right)^n \right] = \ln \left[A_{1100} + c \right] \right\}; \mathbf{V}_{s30} < k_1 \\ (c_{10} + k_2 n) \ln \left(\frac{\mathbf{V}_{s30}}{k_1} \right) \\ (c_{10} + k_2 n) \ln \left(\frac{1100}{k_1} \right) \end{cases}; \mathbf{V}_{s30} < 1100 \end{cases}$$

(from Campbell and Bozorgnia, 2004)

V_{S30} for Regional Site Response Mapping

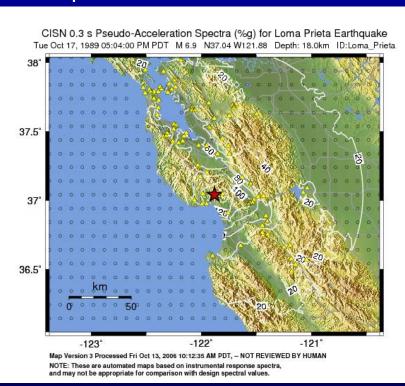
ShakeMaps

$V_{S\,30}$ Map (Topographic Slope) (San Francisco Bay Region)

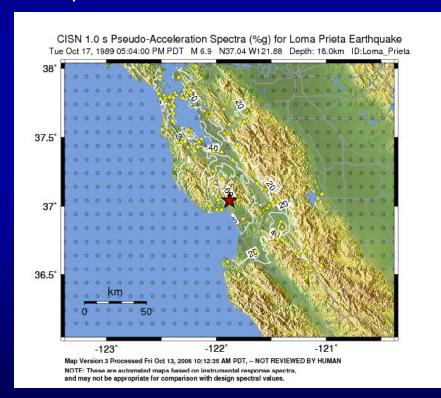


Spectral Acceleration ShakeMaps Loma Prieta Earthquake (San Francisco Bay Region)

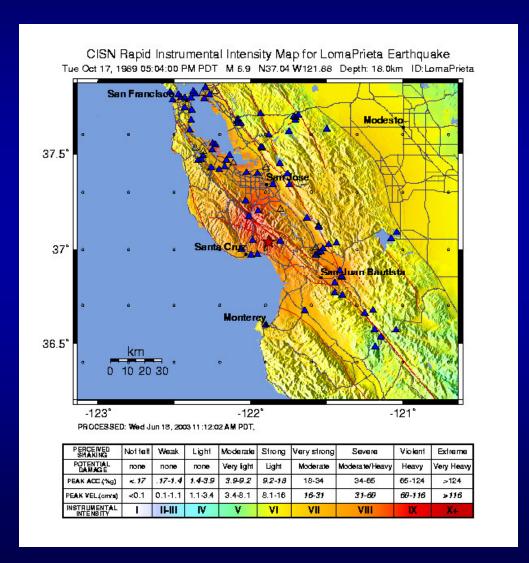
Spectral Acceleration 0.3 Sec



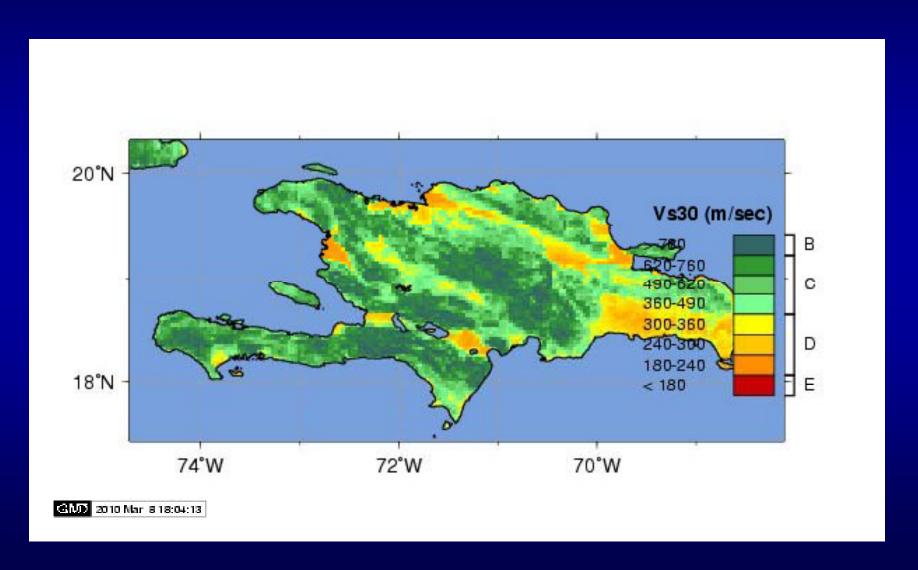
Spectral Acceleration 1.0 Sec



Instrumental Intensity ShakeMap Loma Prieta Earthquake (San Francisco Bay Region)



V_{S30} Map (Topographic Slope) (Haiti Region)

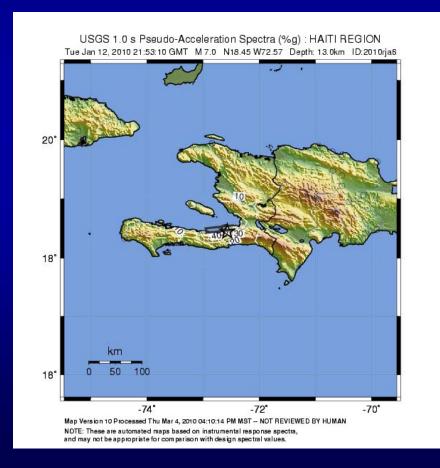


Spectral Acceleration ShakeMaps Tohoku Japan Earthquake M 9.0) (Honshu Japan Region)

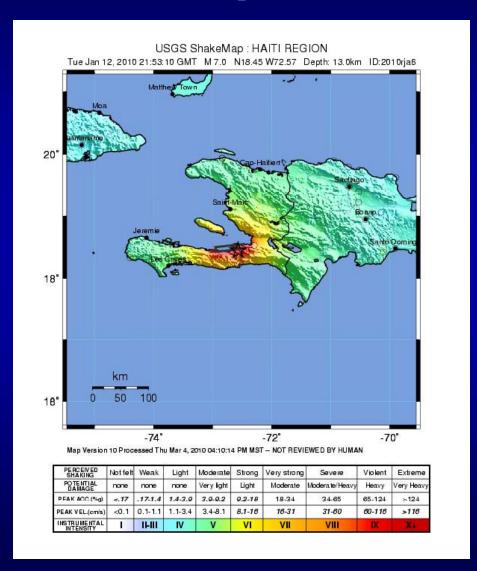
Spectral Acceleration 0.3 Sec

USGS 0.3 s Pseudo-Acceleration Spectra (%g) : HAITI REGION Tue Jan 12, 2010 21:53:10 GMT M 7.0 N18.45 W72.57 Depth: 13.0km ID:2010rja6 18° km 18 -74° Map Version 10 Processed Thu Mar 4, 2010 04:10:14 PM MST - NOT REVIEWED BY HUMAN NOTE: These are automated maps based on instrumental response spectra, and may not be appropriate for comparison with design spectral values.

Spectral Acceleration 1.0 Sec



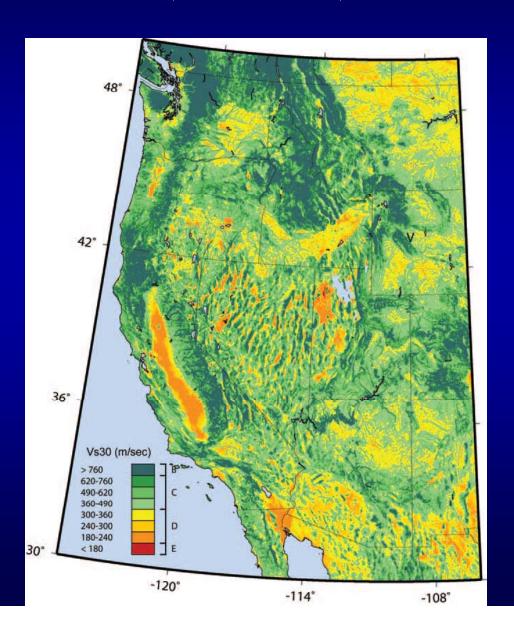
Instrumental Intensity ShakeMap Haiti Earthquake M 7.0)



V_{S30} for Seismic Hazard and Risk Mapping

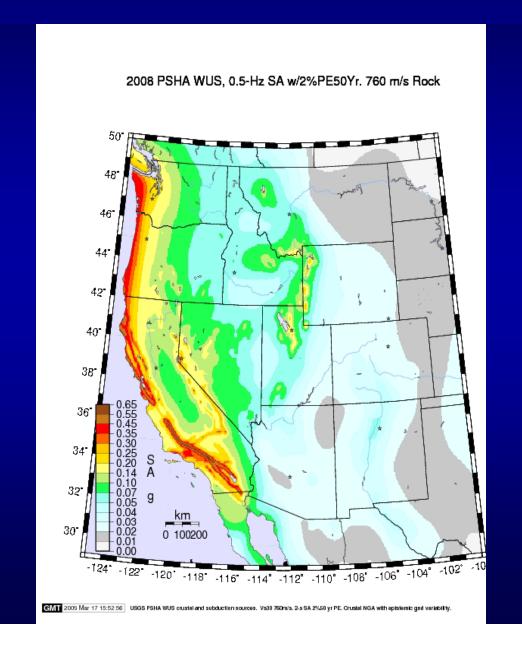
- PSHA Maps
- GEM Global Seismic Hazard Mapping Project

$V_{S\,30}$ Map (Topographic Slope) (Western US)



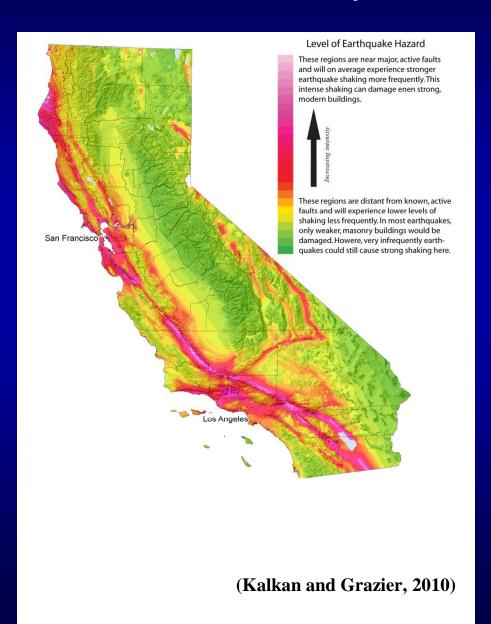
PSHA Map for Rock

(NGA GMPE 2008 SA @2 s, 2% PE 50 yr, $V_{S30} = 760 \text{ m/s}$)



PSHA Map Including Site Conditions (V_{S30})

(SA @1 s, 2% PE 50 yr)



Global GMPE for GEM

(Site condition characterization based on V_{S30})

Global GMPEs for Global Earthquake Model (GEM)





GLOBAL EARTHQUAKE MODEL

Bozorgnia and others, 2011

Conclusions

- Theoretical models and empirical measurements show $V_{S\,30}$ shows a strong correlation with amplification, Fa and Fv, at specific sites.
- Correlations of V_{SZ} with V_{S30} imply V_{SZ} at other depths can be used to predict V_{S30} and amplification, Fa and Fv.
- Correlations of $V_{S\,30}$ with Physical Properties, Geologic Age, and Topographic Slope imply $V_{S\,30}$ can be mapped on regional and global scales.
- Hence, $V_{S\,30}$ serves as a useful basis for characterization of site response for specific sites and for regional mapping purposes for the appropriate applications.
- Important applications of $V_{S,3\theta}$ include:
 - Unambiguous definitions of site classes and site coefficients for routine design in building codes
 - Characterization of site response for GMPEs for use in Site Specific,
 Regional, and Global Mapping of Seismic Hazard for appropriate
 interpretations: ShakeMaps, PSHA Maps, GEM Model